

# 2nd AIAA CFD Drag Prediction Workshop

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Fluent Inc.

Orlando FL, June 21-22, 2003

# DLR-F6 Wing-Body-Nacelle Simulations

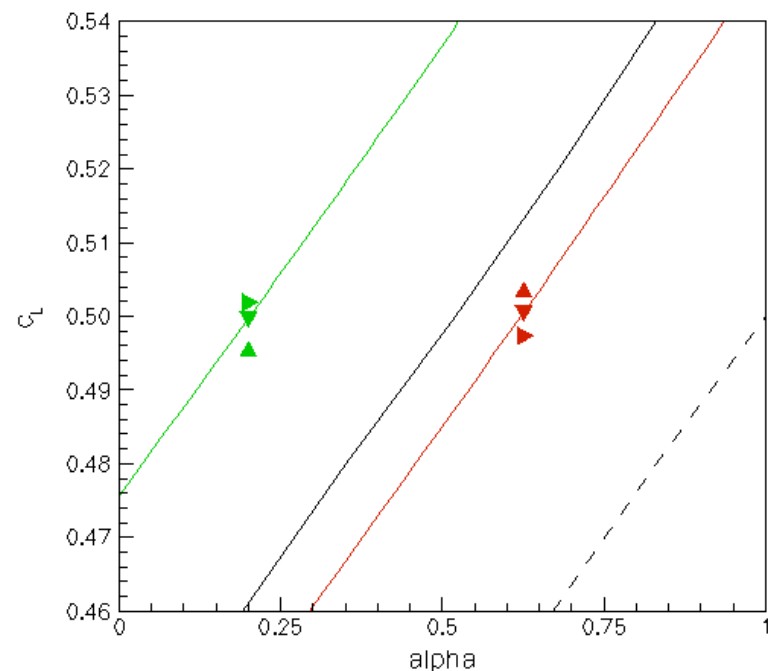
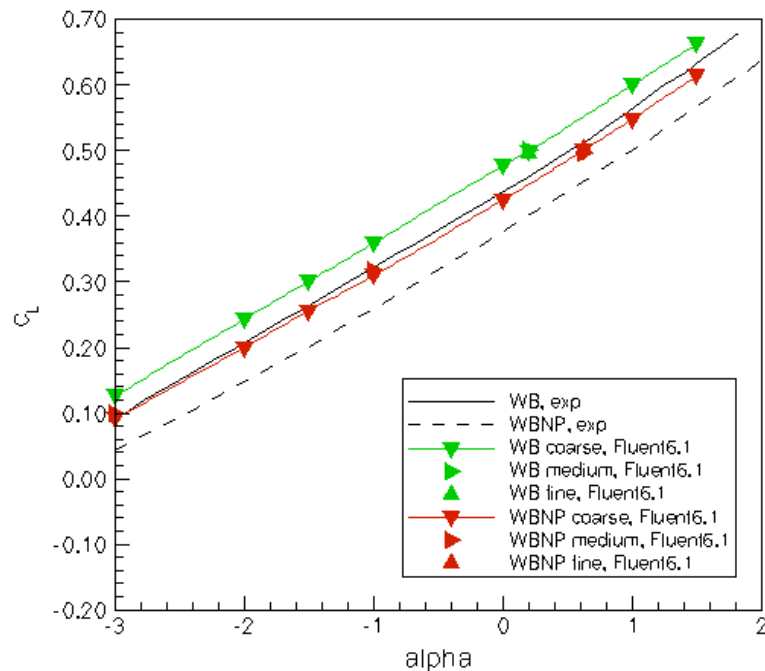
- Fluent 6 - Unstructured solver
- Single point grid sensitivity study for  $M=0.75$ ,  $C_L=0.5$  on provided point-matched ICEM grid
- Drag polar for  $M=0.75$ ,  $Re=3.0 \times 10^6$  on provided point-matched coarse ICEM grid, fully turbulent
- Point-matched structured grid family
- Flow visualization

# Fluent 6 – Solver

- Cell-centered unstructured on hybrid meshes
- Segregated implicit (pressure based, SIMPLE) and coupled implicit (density based) solver
  - Segregated solver requires 11GB for 13.5M cell fine WBNP case, fits on 8 node Linux cluster with 16GB of RAM
  - Coupled solver doubles the memory requirements, requires more resources
- Second-order upwind reconstruction
- Cell- or node-based gradient calculation
- Algebraic Multigrid
- Realizable k- $\epsilon$  turbulence model
- Two-layer zonal model for wall treatment

# Single Point Grid Sensitivity: $C_L(\alpha)$

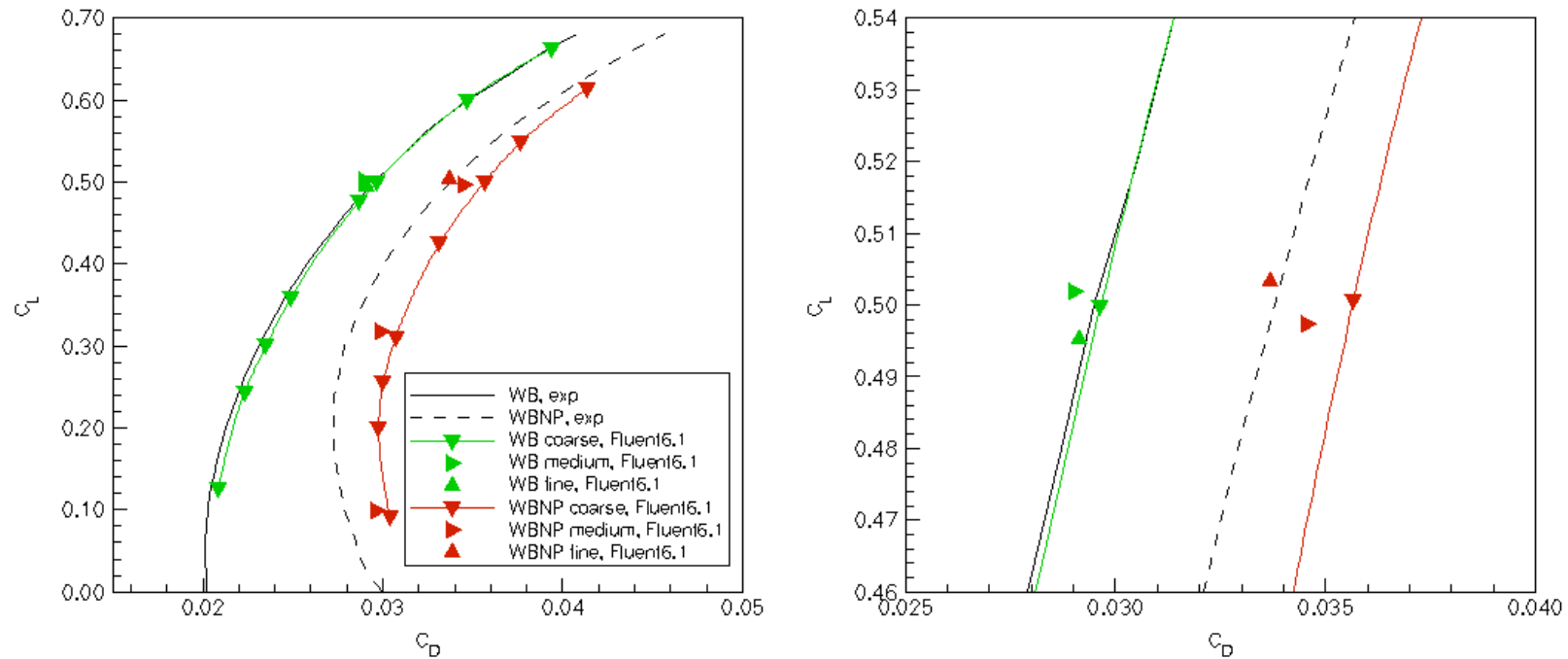
$M=0.75$ ,  $Re=3.0 \times 10^6$ , segregated node-based solver



- WB coarse:  $C_L=0.500$  at  $\alpha=0.2007^\circ$
- WBNP coarse:  $C_L=0.500$  at  $\alpha=0.6263^\circ$
- Medium and fine grid runs at fixed angles of attack obtained from coarse grids
- $C_L(\alpha)$  not monotonically increasing or decreasing as grid is refined

# Single Point Grid Sensitivity: $C_L(C_D)$

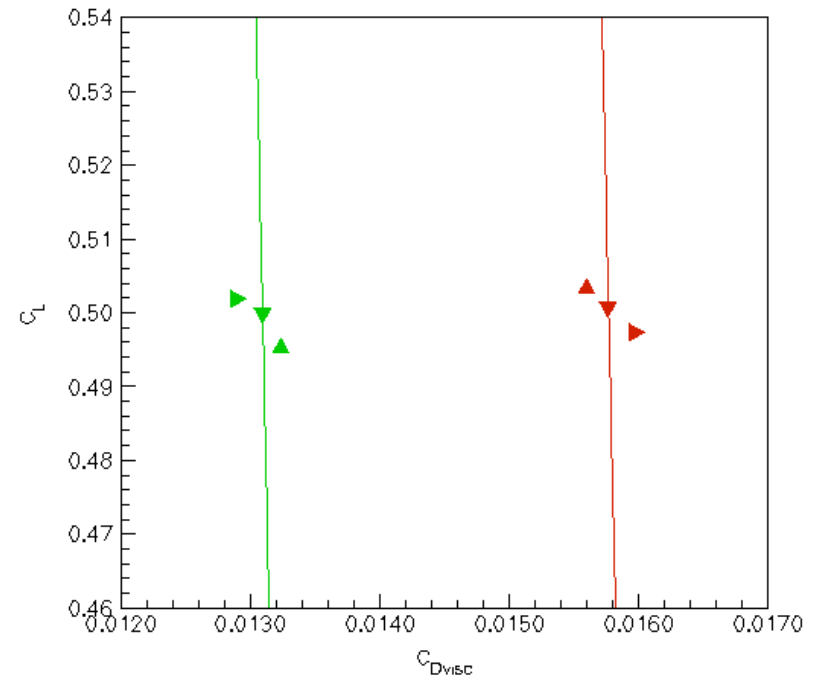
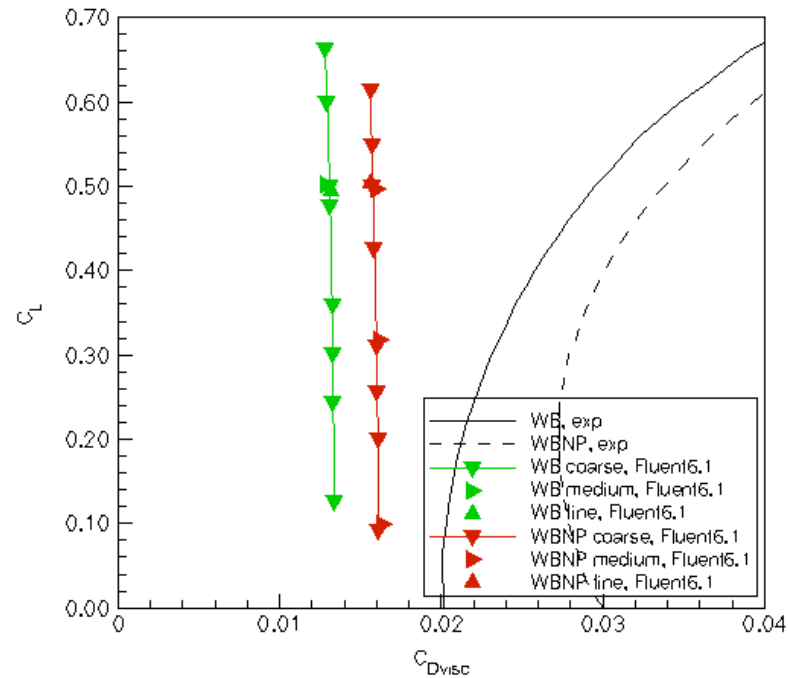
$M=0.75$ ,  $Re=3.0 \times 10^6$ , segregated node-based solver



- Deviation in  $C_L$  of 0.001 due to fixed angle of attack corresponds at  $C_L=0.5$  to deviation in  $C_D$  of less than 0.5 drag counts
- Monotonic  $C_D$  reduction for WBNP with mesh refinement
- Non-monotonic  $C_D$  for WB as mesh is refined

# Single Point Grid Sensitivity: $C_L(C_{Dvisc})$

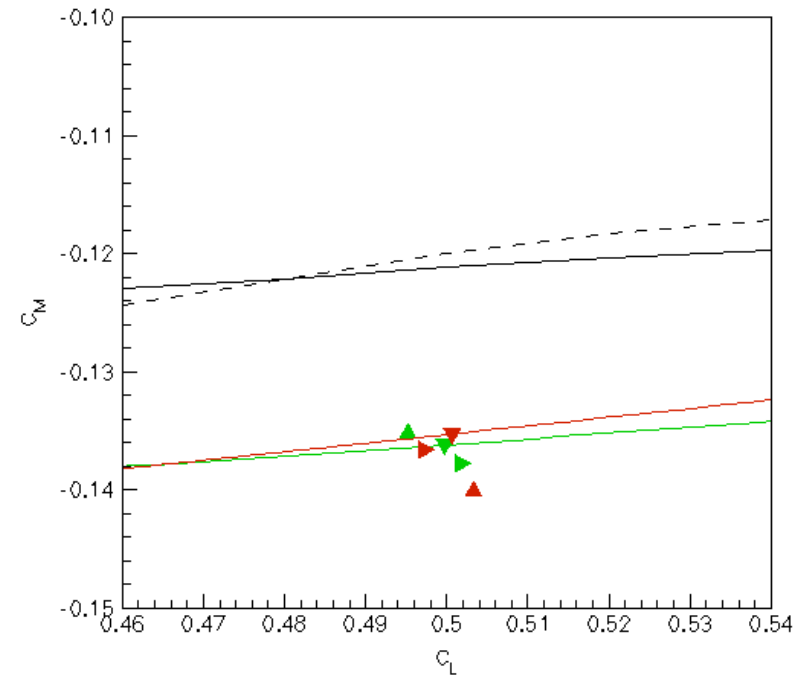
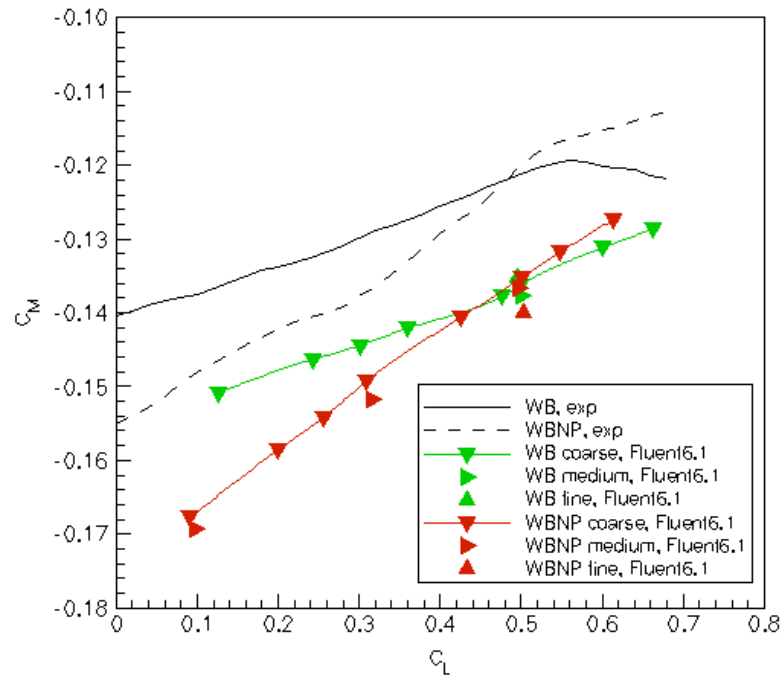
$M=0.75$ ,  $Re=3.0 \times 10^6$ , segregated node-based solver



- Viscous drag component  $C_{Dvisc}$  not monotonic with grid refinement

# Single Point Grid Sensitivity: $C_M(C_L)$

$M=0.75$ ,  $Re=3.0 \times 10^6$ , segregated node-based solver



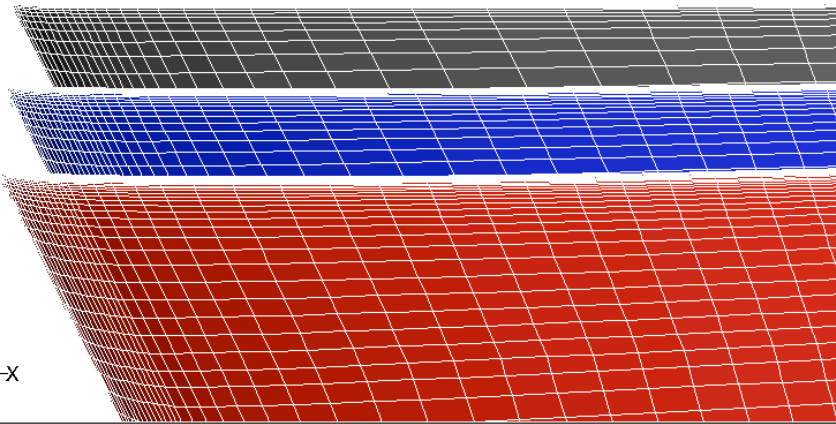
-Too large downward pitching moment for both WB and WBNP

- $C_M$  not monotonic with mesh refinement for WB

# Single Point Grid Sensitivity

ICEM grids at wing root: coarse, medium, fine

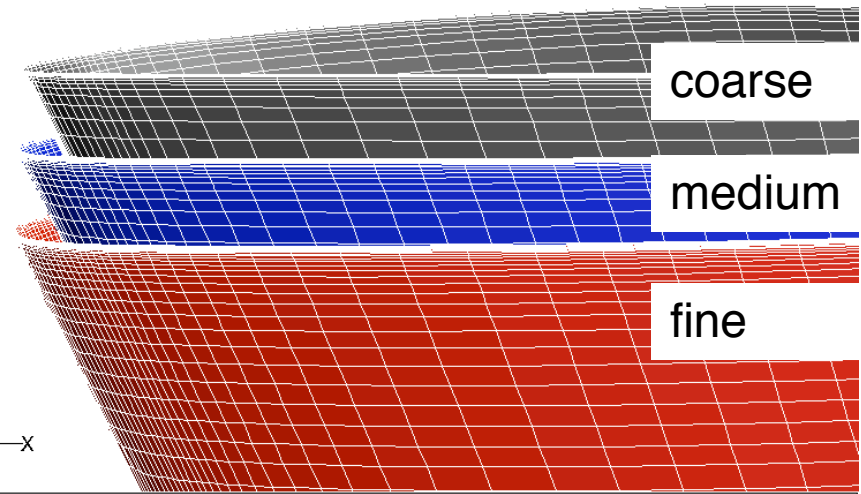
WB



Mesh  
Restrictions:

Jun 19, 2003  
TGrid 3.5 (3D)

WBNP



Mesh  
Restrictions:

Jun 19, 2003  
TGrid 3.5 (3D)

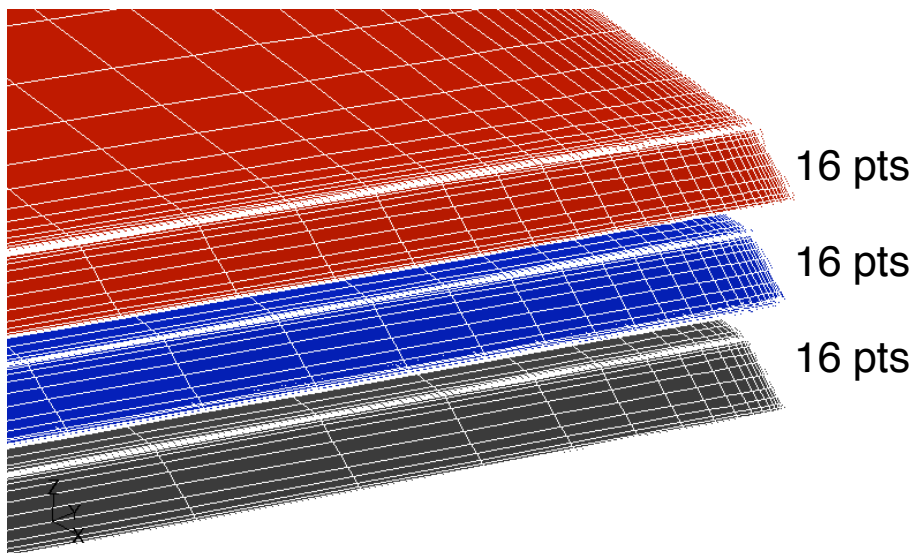
- Nonuniform streamwise refinement
- Medium surface grid locally often finer than fine grid



# Single Point Grid Sensitivity

ICEM grids at trailing edge: coarse, medium, fine

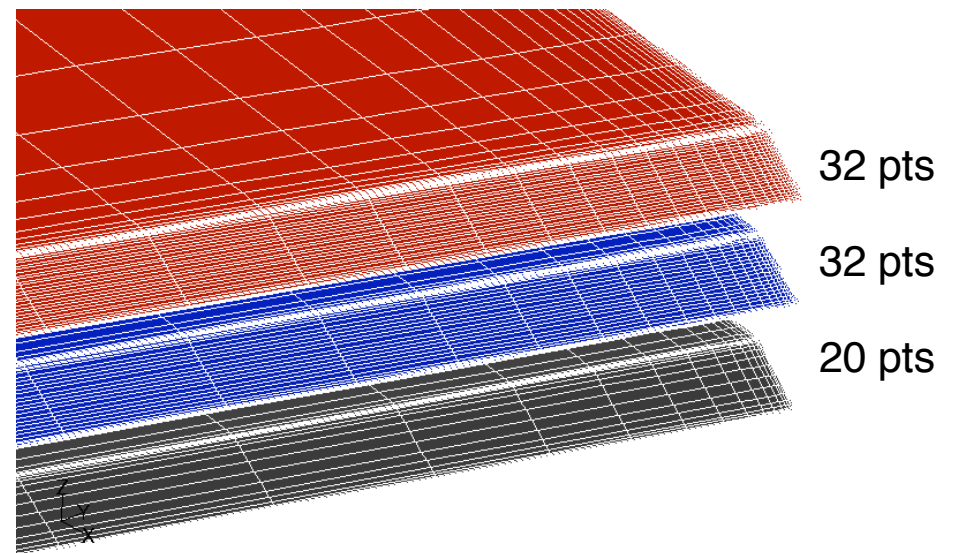
WB



Mesh  
Restrictions:

Jun 19, 2003  
TGrid 3.5 (3D)

WBNP



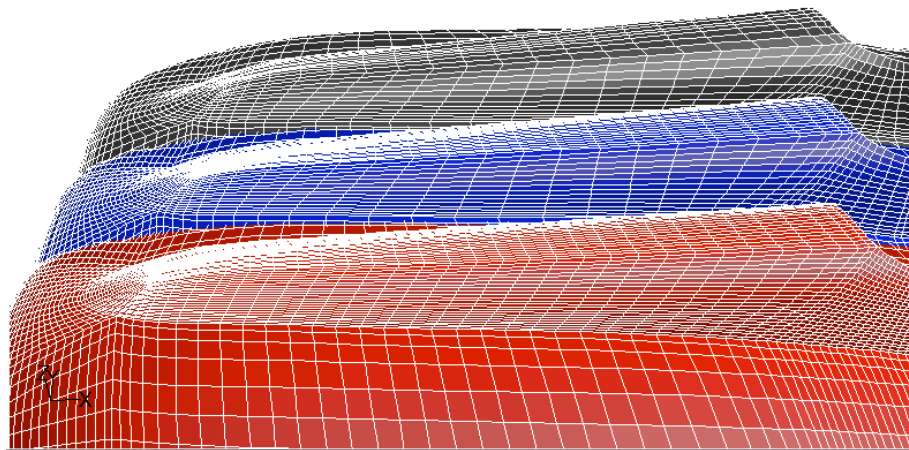
Mesh  
Restrictions:

Jun 19, 2003  
TGrid 3.5 (3D)

- Irregular trailing edge refinement

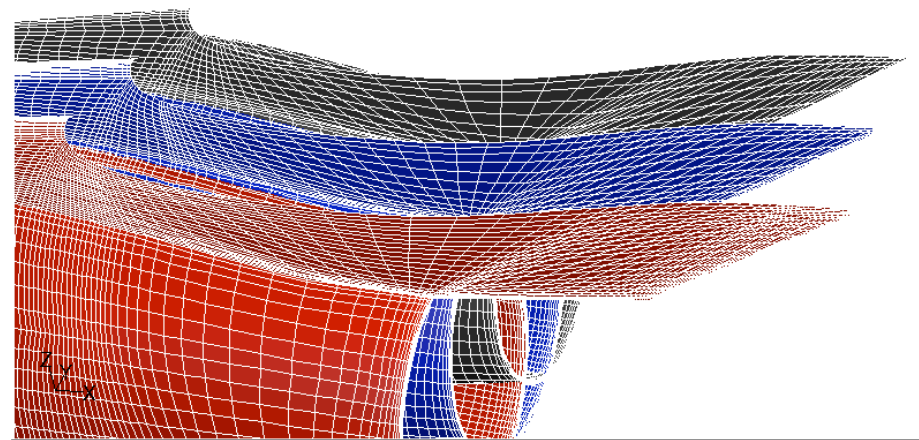
# Single Point Grid Sensitivity

ICEM grids (WBNP) at nacelle, pylon: coarse, medium, fine



Mesh  
Restrictions:

Jun 19, 2003  
TGrid 3.5 (3D)

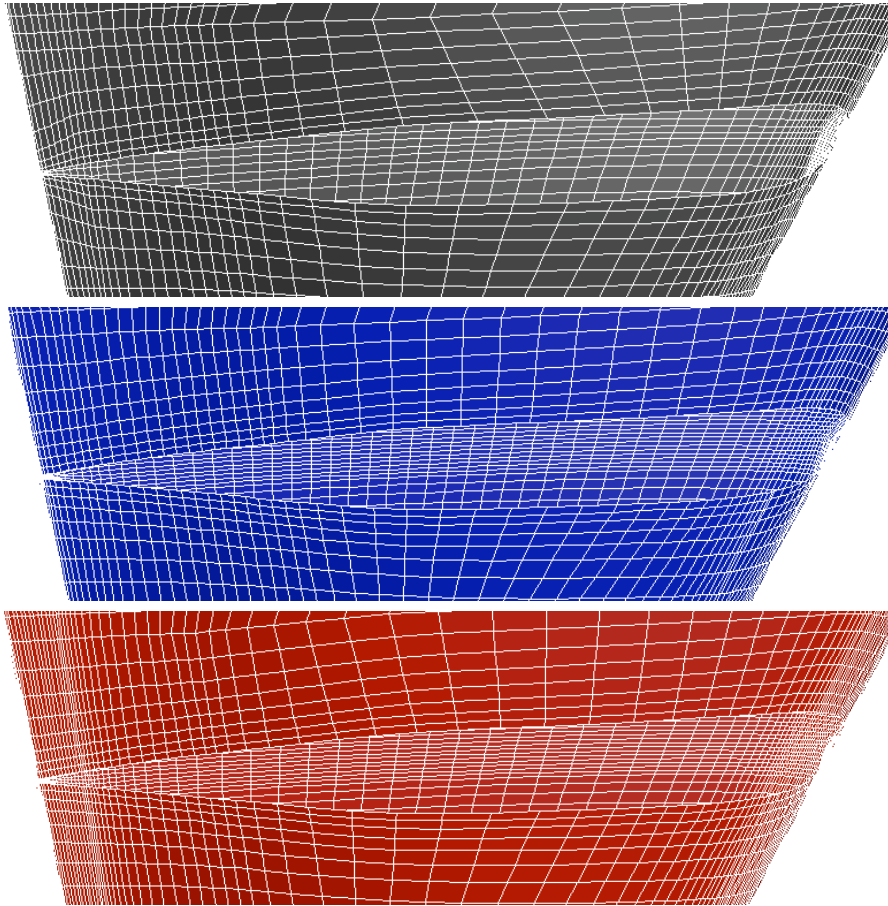


Mesh  
Restrictions:

Jun 19, 2003  
TGrid 3.5 (3D)

# Single Point Grid Sensitivity

ICEM grids (WBNP) at bottom wing: coarse, medium, fine



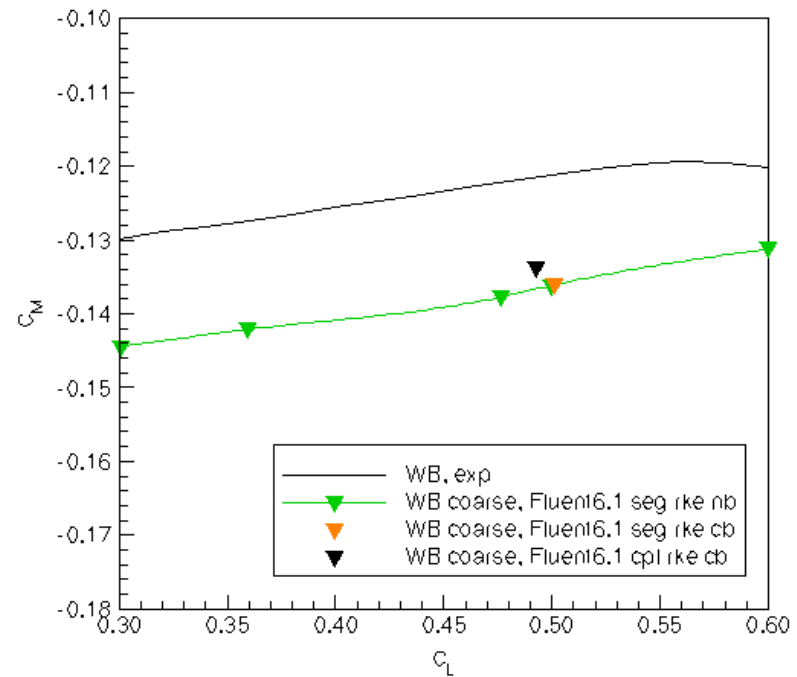
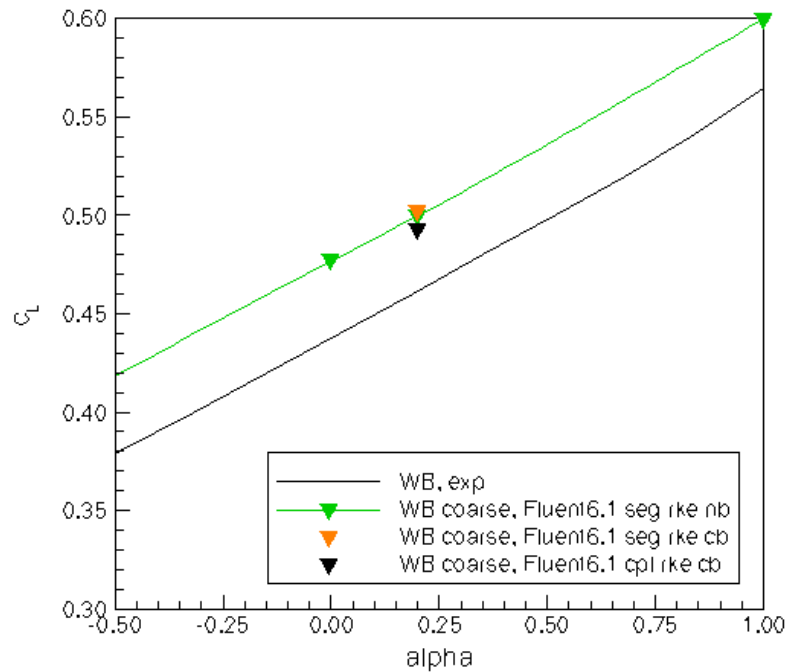
- Medium surface grid is locally often finer than fine grid
- Refinement levels considerably lower than gridding guidelines (e.g. fine WB wing surface mesh has only 17% more elements than medium WB wing)
- Are results still expected to be monotonic with grid refinement?

# WB coarse grid: $C_L(\alpha)$ and $C_M(C_L)$

$M=0.75$ ,  $Re=3.0 \times 10^6$

Solver: Segregated (seg) vs. Coupled (cpl)

Discretization: node-based (nb) vs. cell-based (cb)

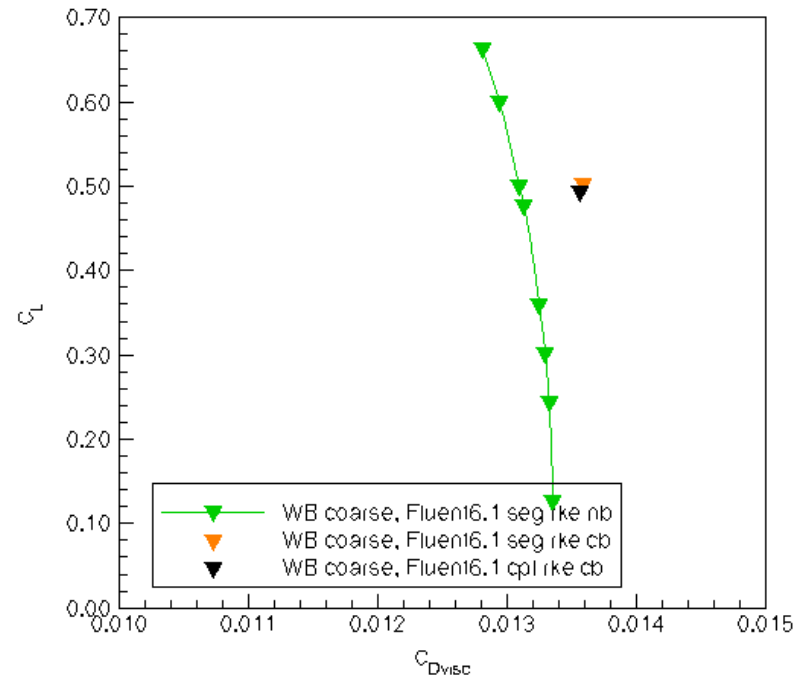
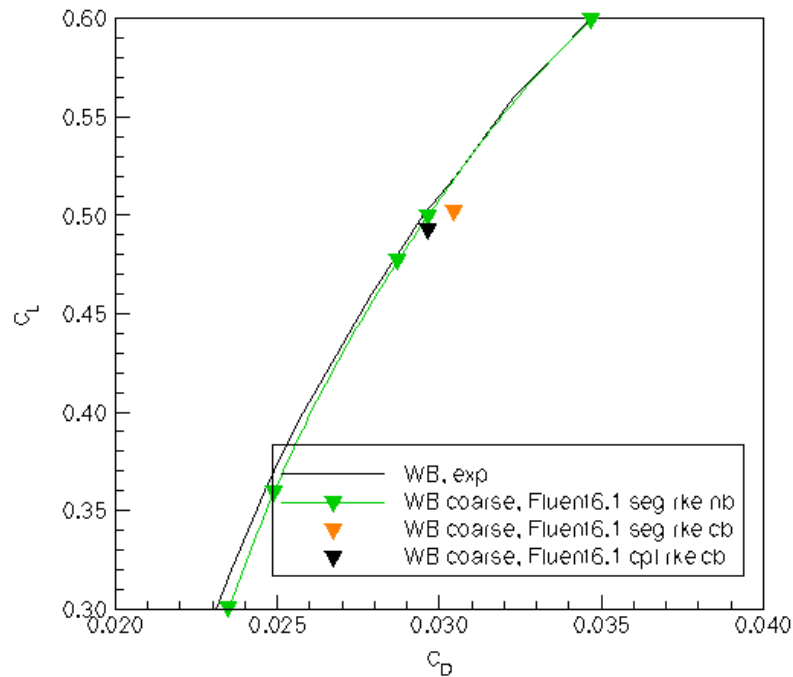


# WB coarse grid: $C_L(C_D)$ and $C_L(C_{Dvisc})$

$M=0.75$ ,  $Re=3.0 \times 10^6$

Solver: Segregated (seg) vs. Coupled (cpl)

Discretization: node-based (nb) vs. cell-based (cb)

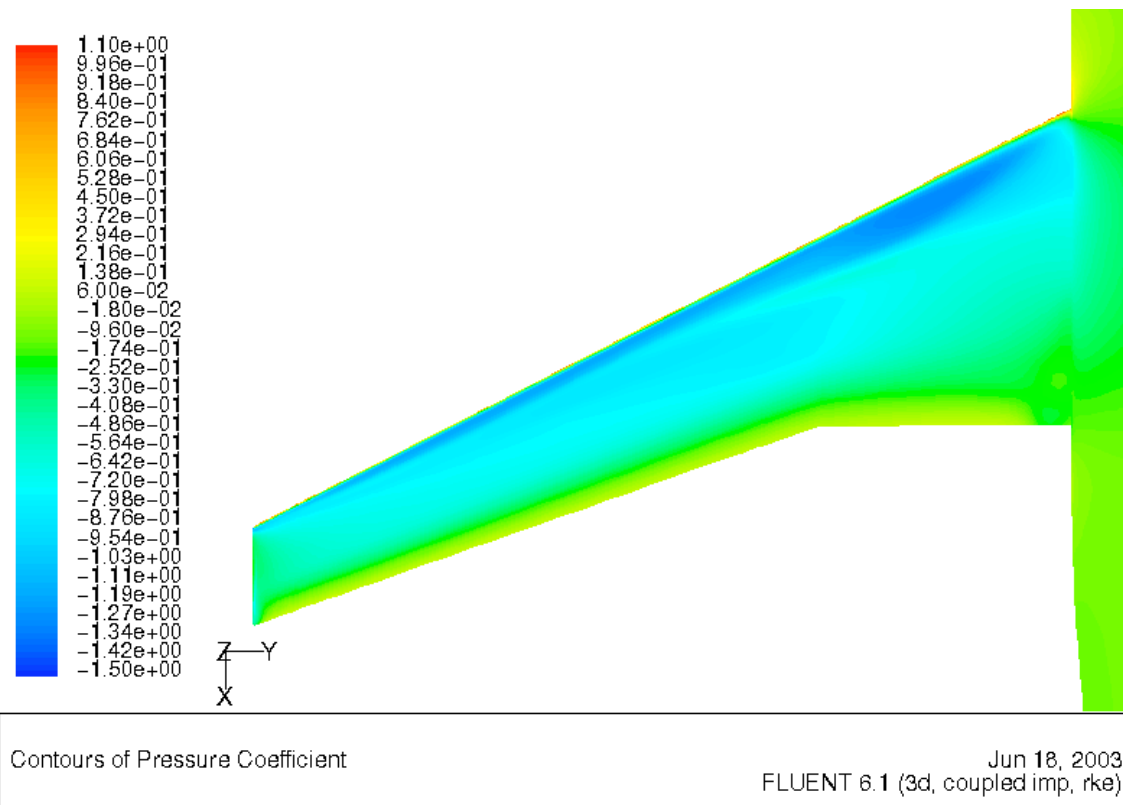


-  $C_{Dvisc}$  increased by 5 counts for cell-based solver

# WB coarse grid: $C_p$

$M=0.75$ ,  $Re=3.0 \times 10^6$ ,  $\alpha=0.2007^\circ$ ,  $C_L=0.493$

Coupled cell-based solver

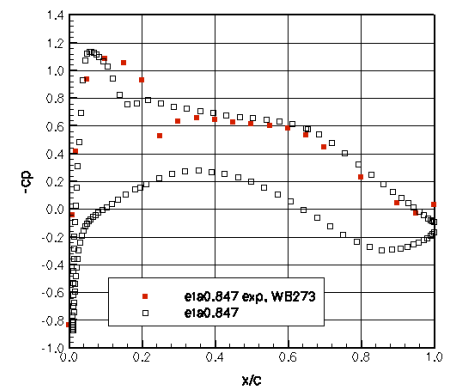
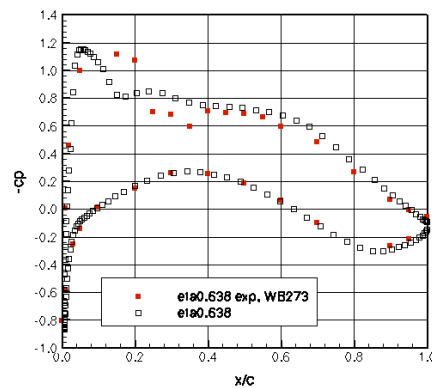
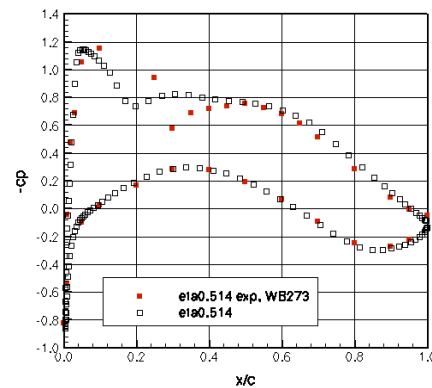
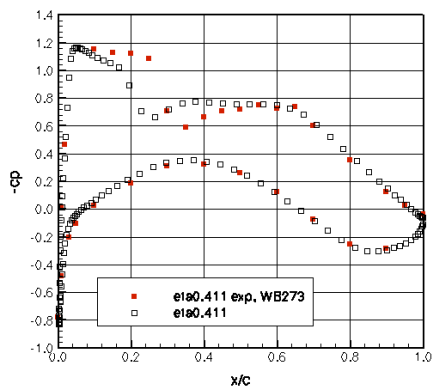
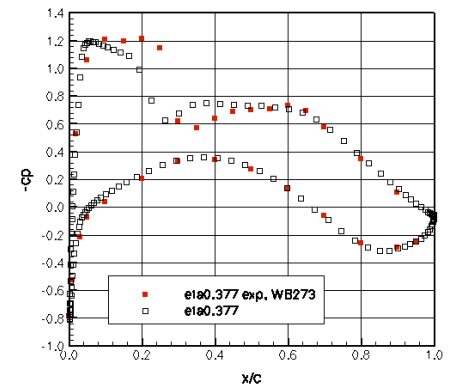
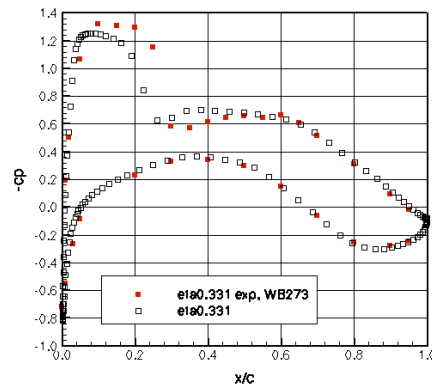
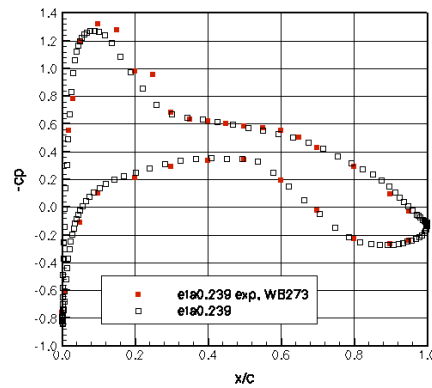
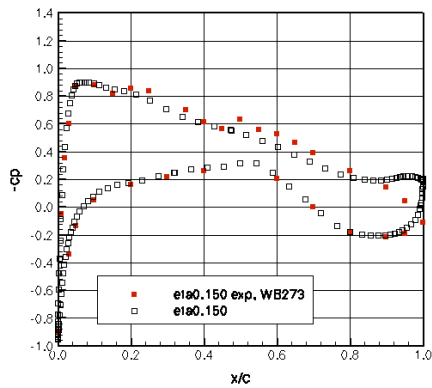


# WB coarse grid: $C_p$

$M=0.75$ ,  $Re=3.0 \times 10^6$ ,  $\alpha=0.2007^\circ$ ,  $C_L=0.493$

Experiments at  $\alpha=0.490^\circ$ ,  $C_L=0.4984$

Coupled cell-based solver



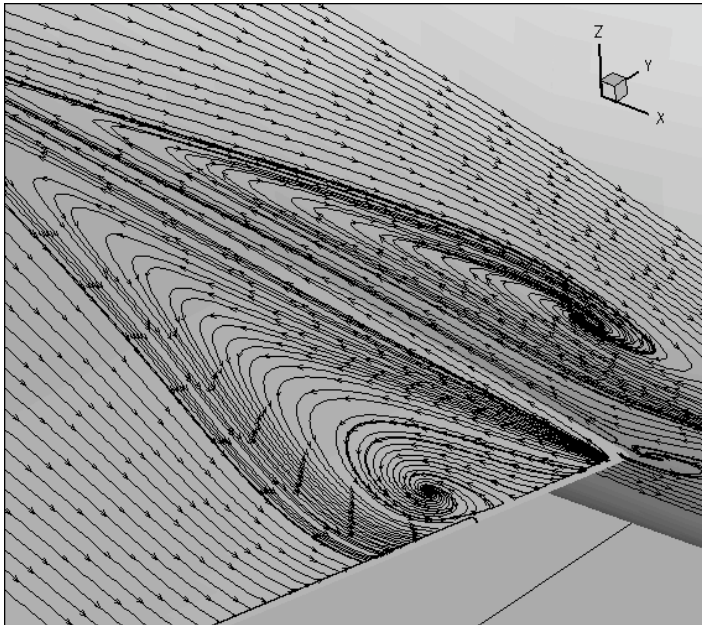


# Flow separation at wing root

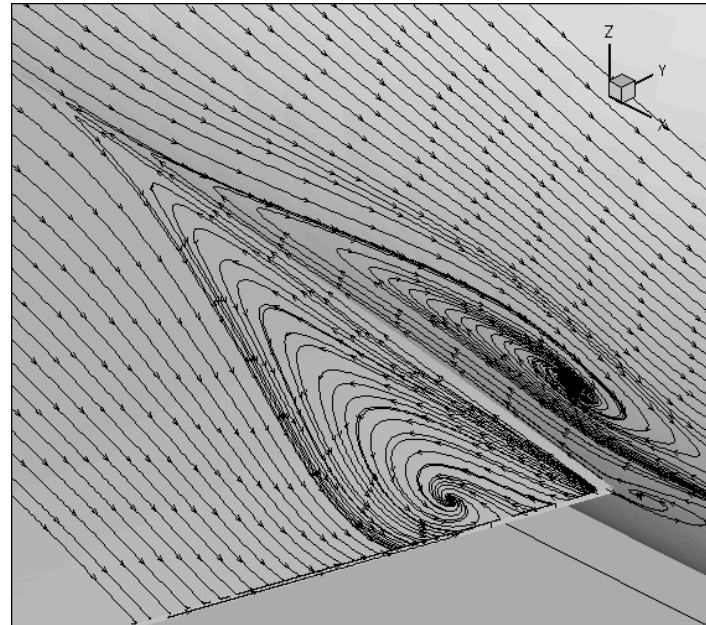
$M=0.75$ ,  $Re=3.0 \times 10^6$ ,  $\alpha=0.2007^\circ$

Segregated node-based solver

WB fine grid



WBNP fine grid



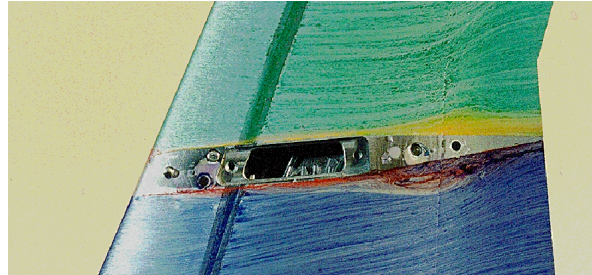
- $BL_{BUB}$  not available due to missing saddle point near trailing edge
- $FS_{BUB}$  difficult to measure



# Streamlines at pylon-wing junction

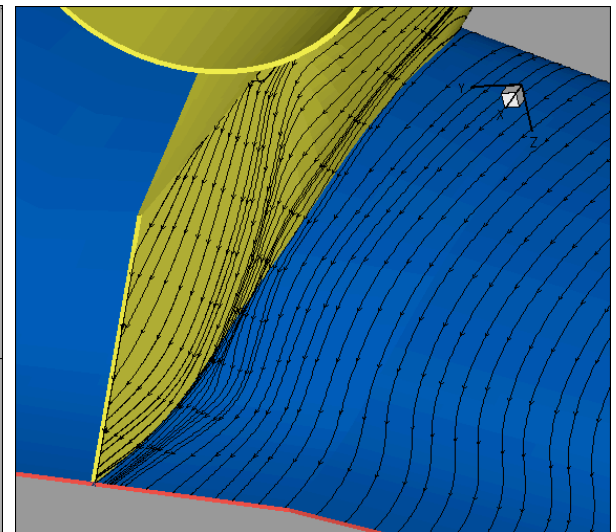
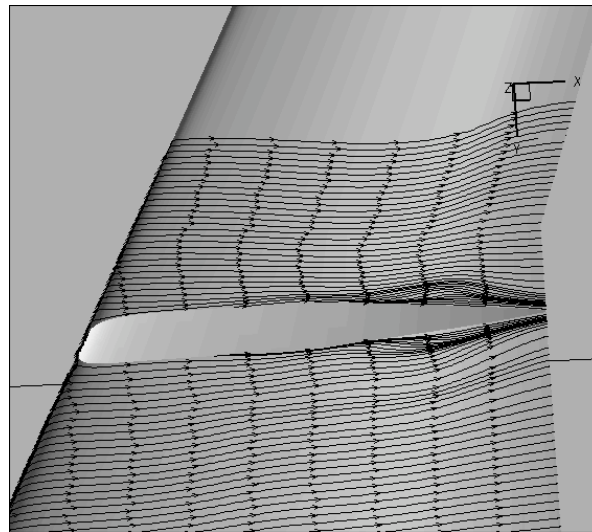
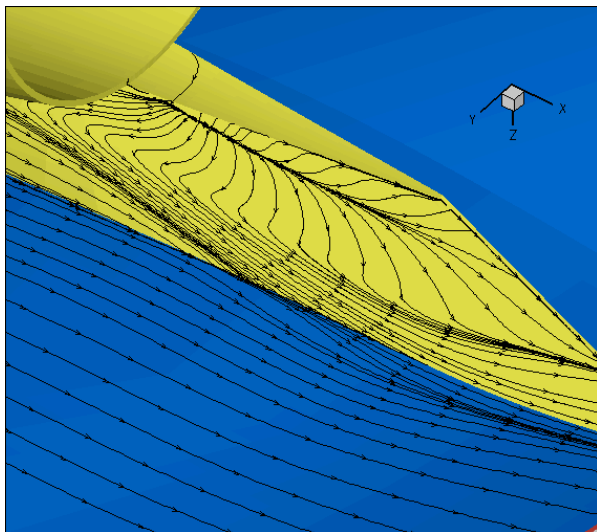
$M=0.75$ ,  $Re=3.0 \times 10^6$ ,  $\alpha=0.6263^\circ$

Segregated node-based solver, WBNP fine grid



Inboard pylon

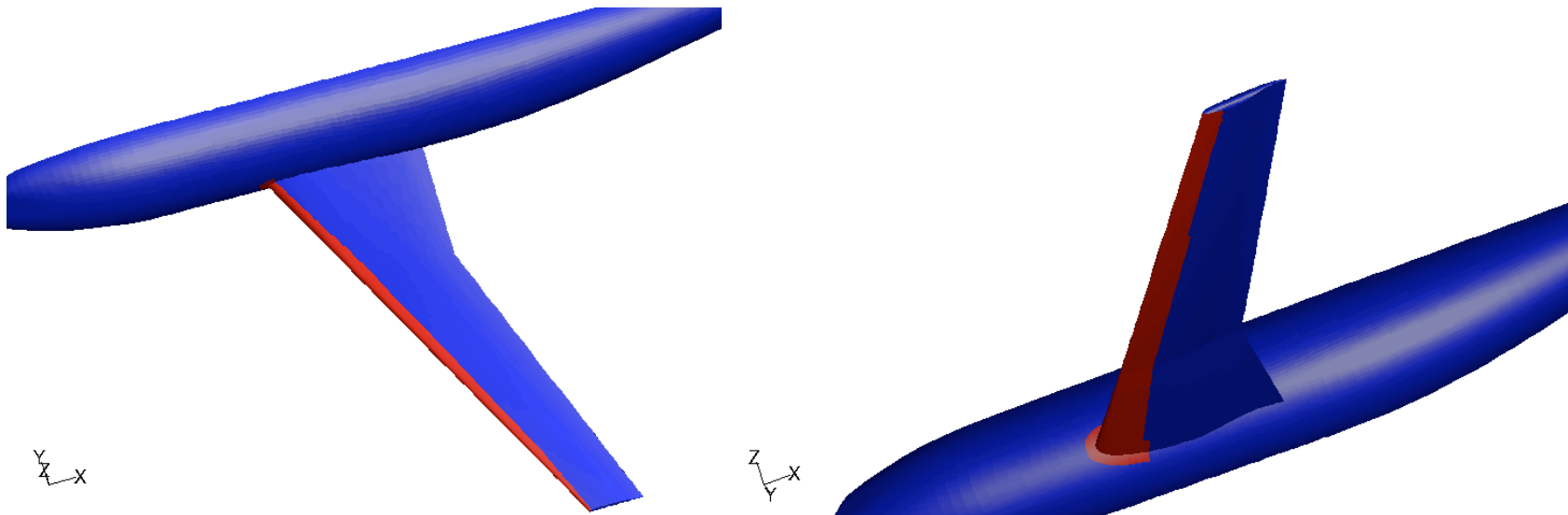
Outboard pylon



- No separation on lower wing surface near pylon

# Transition location specification

- Laminar zone option in Fluent to model transition
- Not used for DPW2 calculations



# Summary

- Overprediction of lift very similar to DLR-F4 case of DPW1
- Good match of drag polar, despite unsatisfactory match of  $c_p$  distribution in vicinity of shock
- Poor match of pitching moments
- Good quality grids are essential
  - Distributed point-matched structured grid family has poor and inconsistent refinement
  - Even the fine mesh doesn't capture the shock locations properly
  - A proper grid refinement study requires a parametrically refined family of grids
  - Efficient use of grid points is critical for economics
  - Grid generation of multi-block structured grids is still a bottleneck
- Coupled (density based) solver in Fluent 6 recommended for transonic drag predictions on marginally resolved grids