

# DPW-8 & AePW-4

## Static Deformation Working Group

January 17, 2025

[dpwaiaa@gmail.com](mailto:dpwaiaa@gmail.com)

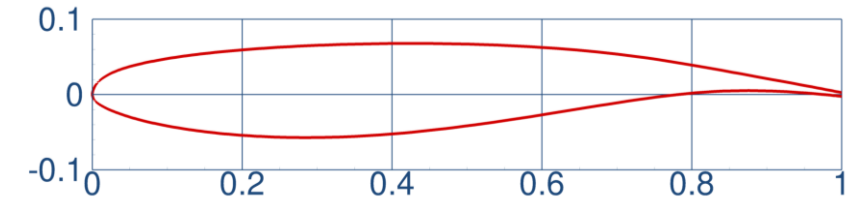
(working group specific email TBD)



- **Meeting schedule**
  - Third Friday of the month; 10:00 Eastern Time (will adjust with US Daylight Saving Time)
- **For questions about the working group, please email [dpwaiiaa@gmail.com](mailto:dpwaiiaa@gmail.com)**
- **Websites**
  - Static Deformation Working Group website  
<https://aiaa-dpw.larc.nasa.gov/WorkingGroups/Group2/group2.html>
  - Geometry/Grid websites  
<https://aiaa-dpw.larc.nasa.gov/geometry.html>  
<https://aiaa-dpw.larc.nasa.gov/grids.html>
  - Postprocessing website (including ONERA OAT15A experimental results)  
<https://aiaa-dpw.larc.nasa.gov/postprocessing.html>
  - Large File Upload  
<https://nasagov.app.box.com/f/fd164563283b4e85857d1a0975b0b363>

# Test Case 1a: Workshop-Wide Validation

- **Validation of steady CFD analysis, required**
- **Users are encouraged to employ best practices**
- **Settings**
  - Steady CFD (e.g., RANS)
  - Prefer some version of SA, multiple turbulence models can be submitted
  - Purely 2D simulations (one cell wide)
- **Grids**
  - Six-member RANS grid family; four are required, six are desirable
  - Encourage use of committee-supplied grids; user-generated grids are acceptable
  - Committee-supplied grid is one cell wide with a 230mm chord (same as experiment) and follows RANS best practices
- **Conditions**
  - Mach 0.73,  $Re_c=3m$  (based on chord length),  $T_{static} = 271 \text{ K (487.8 R)}$
  - Alpha: 1.36, 1.50, 2.50, 3.00, 3.10

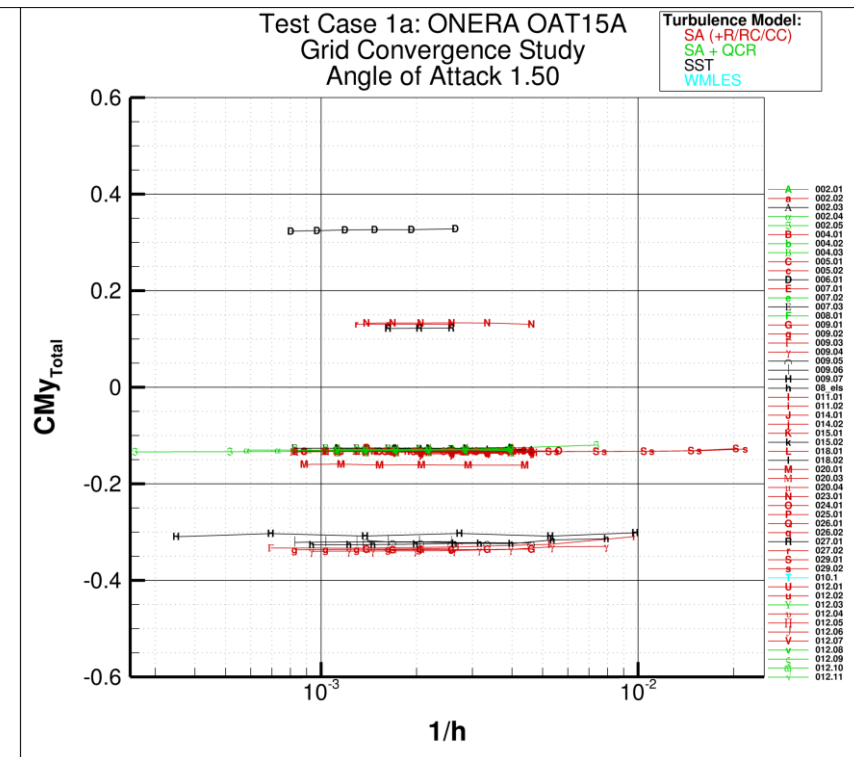
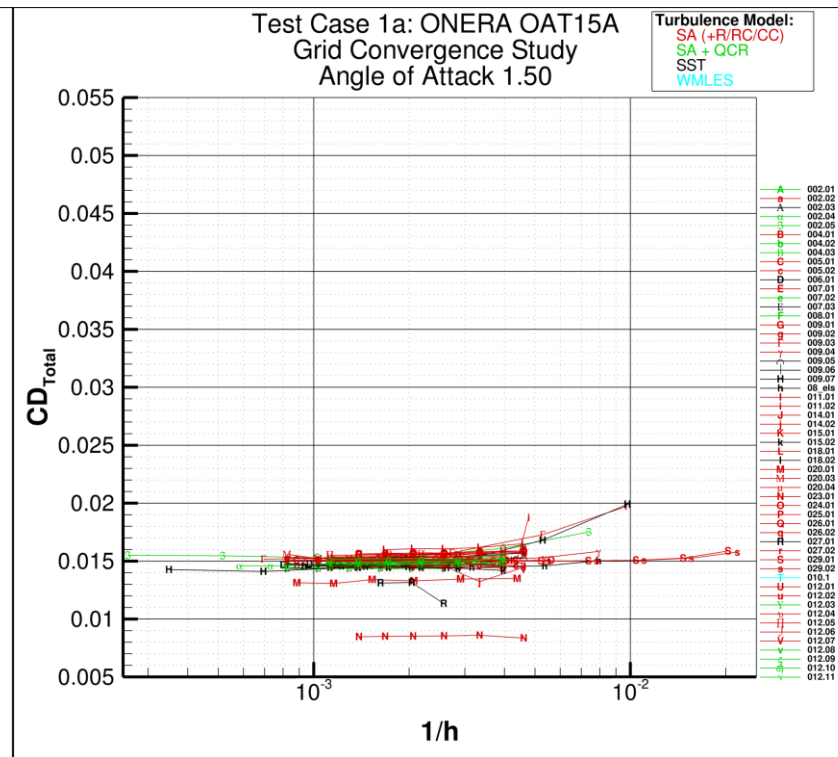
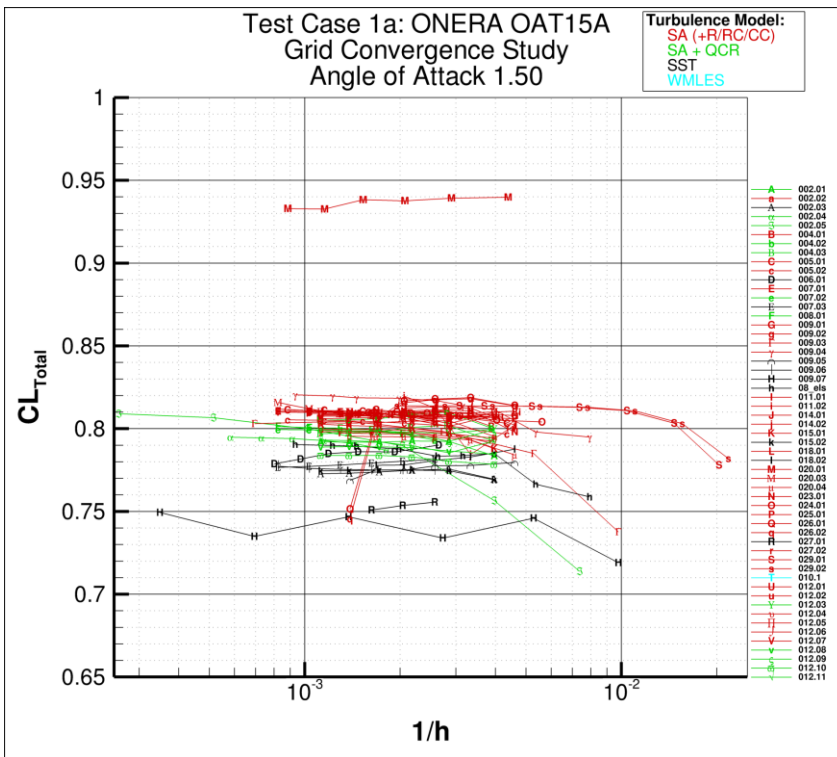


ONERA OAT15A Transonic Airfoil

Jaquin, et al. "Experimental Study of Shock Oscillation over a Transonic Supercritical Profiles." AIAA Journal, Vol. 47, No. 9, 2009. Pages 1985-1994.

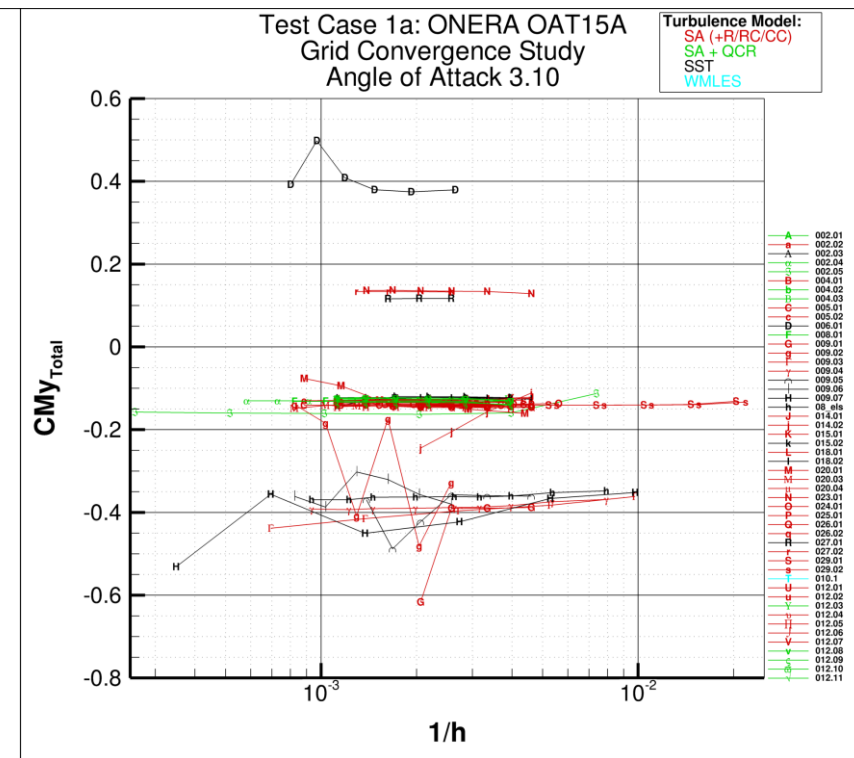
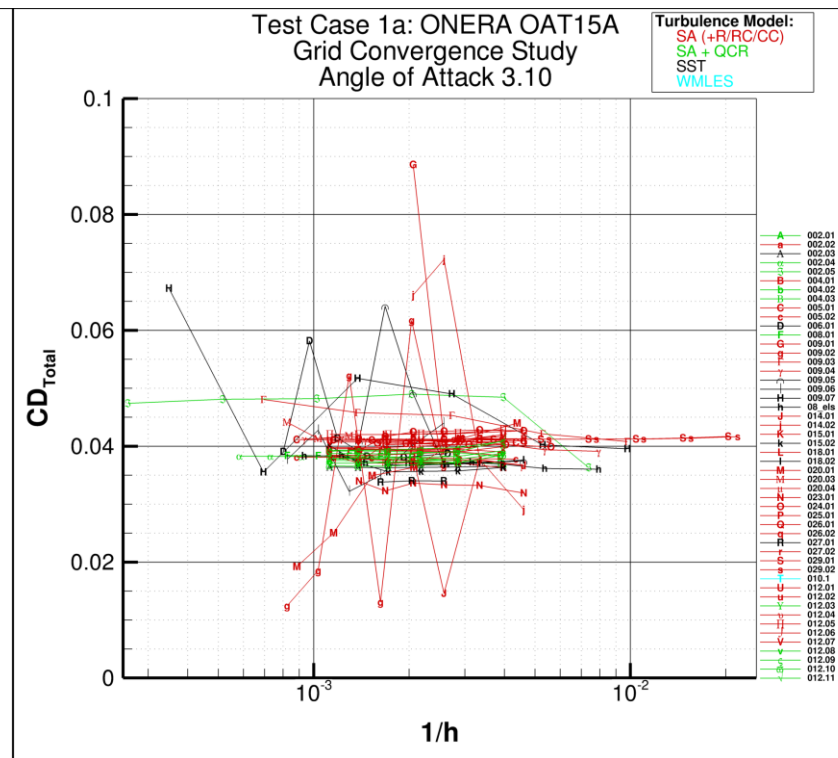
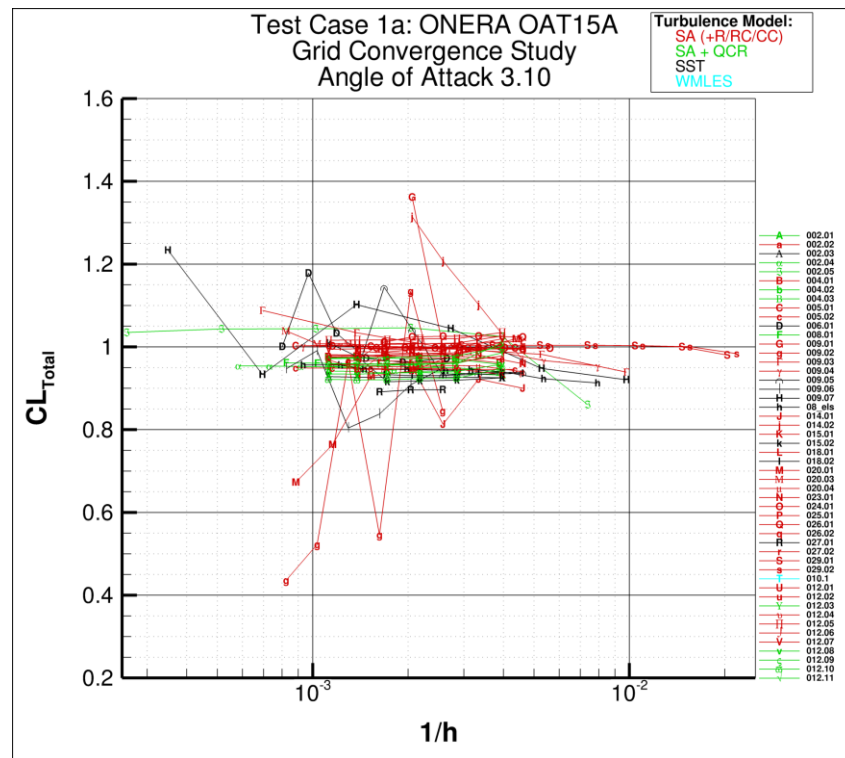
# Test Case 1a: Results

- Grid Convergence Study
  - Alpha = 1.50°



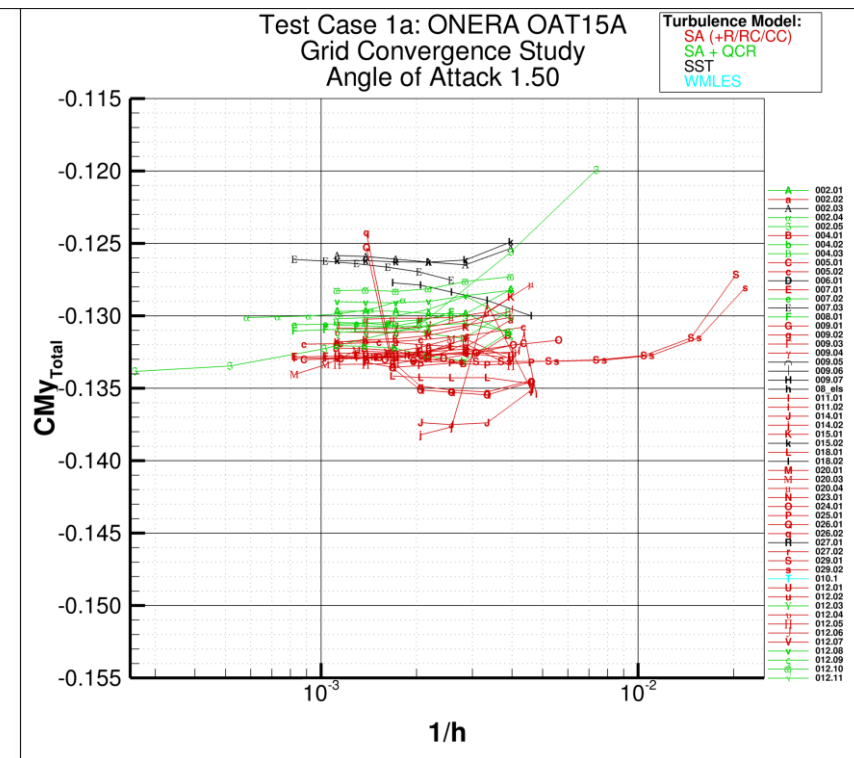
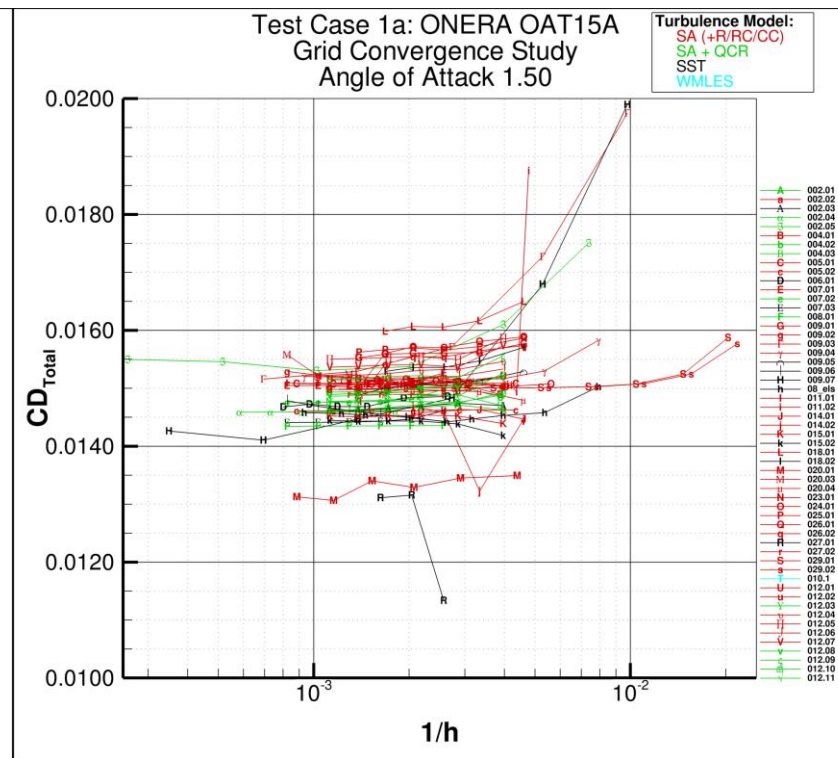
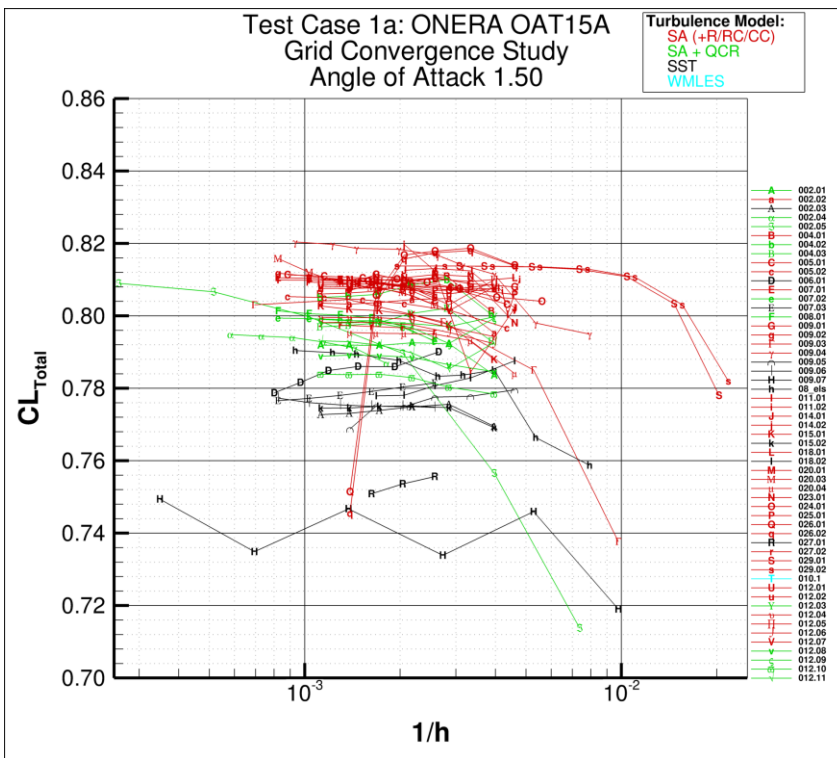
# Test Case 1a: Results

- Grid Convergence Study
  - Alpha = 3.10°



# Test Case 1a: Results

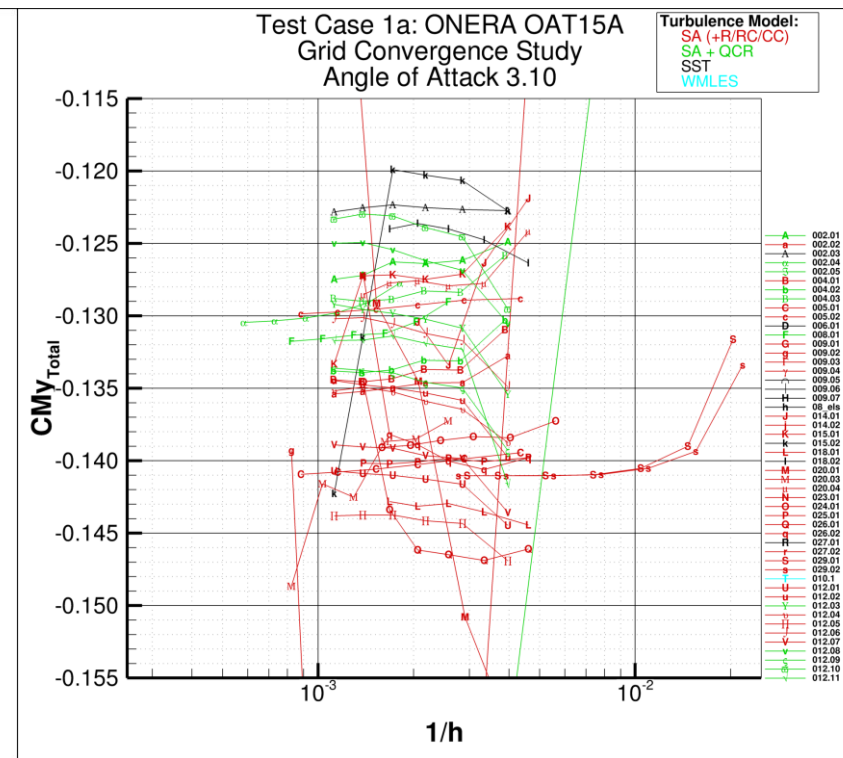
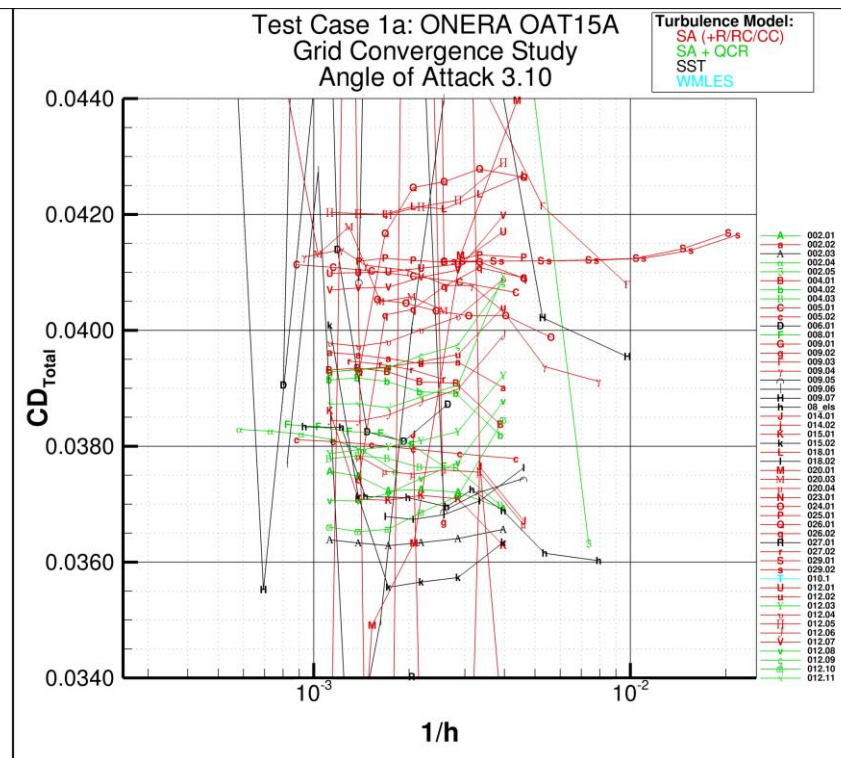
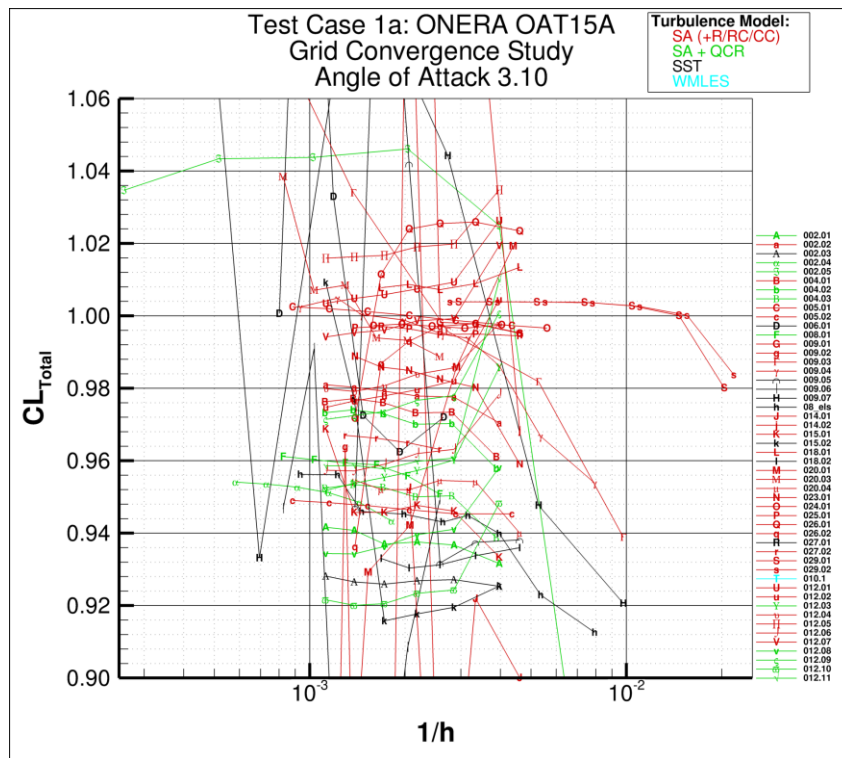
- Grid Convergence Study
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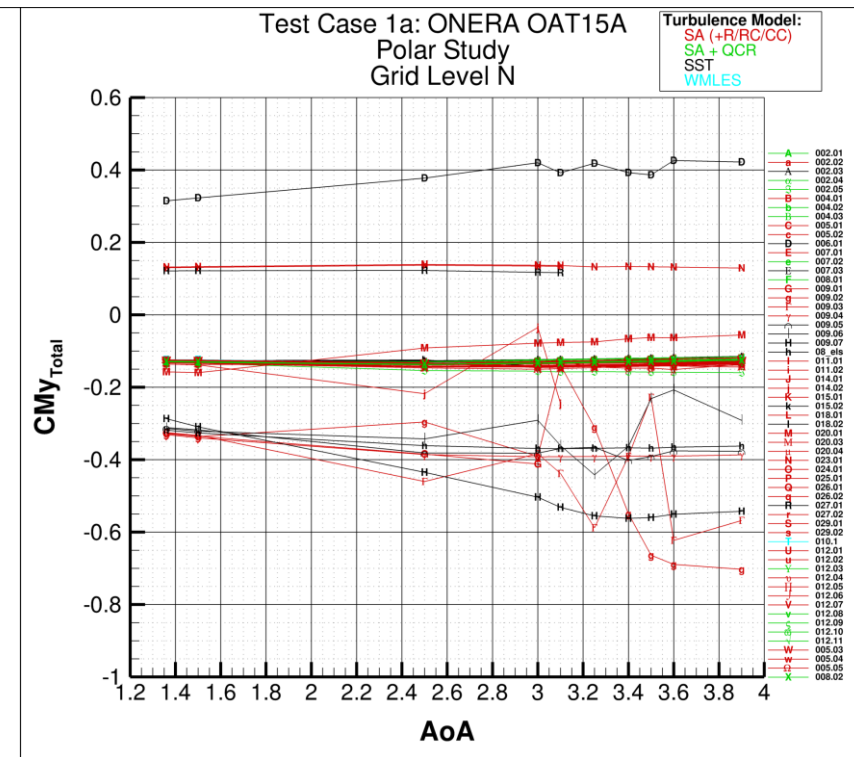
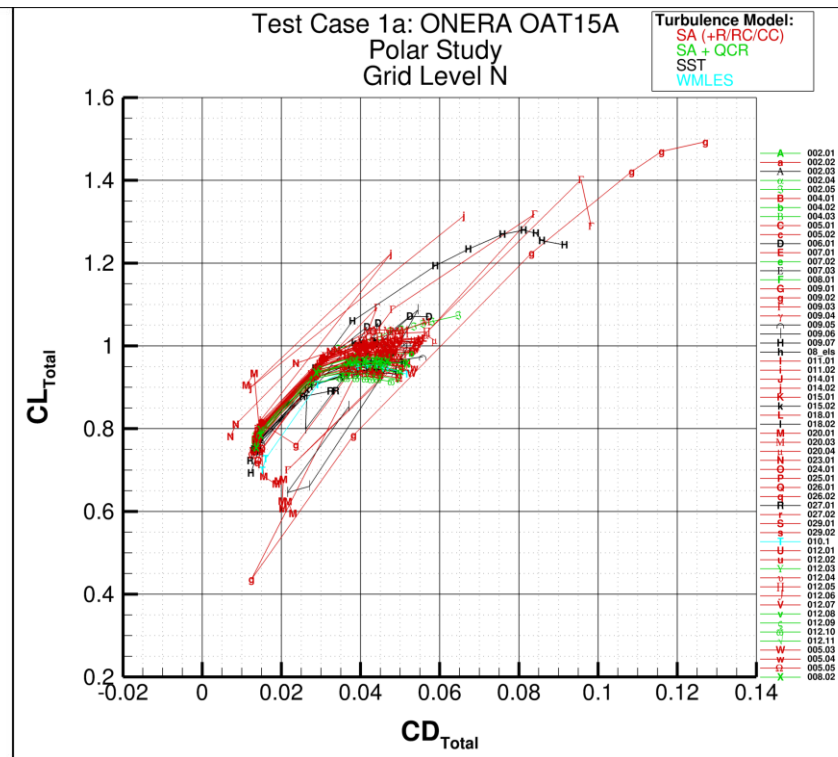
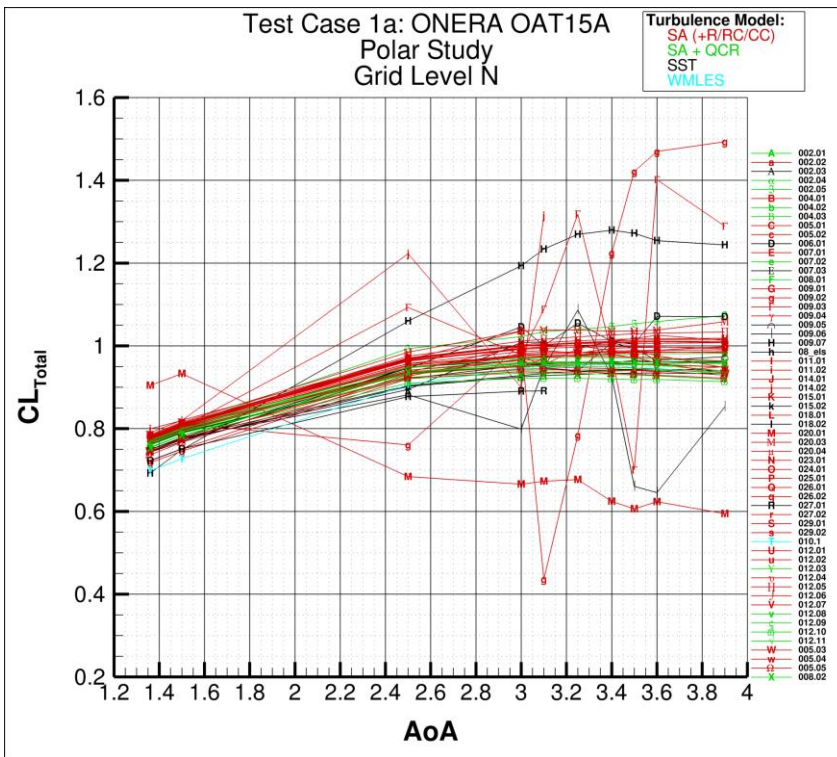
# Test Case 1a: Results

- Grid Convergence Study
  - Alpha = 3.10°



# Test Case 1a: Results

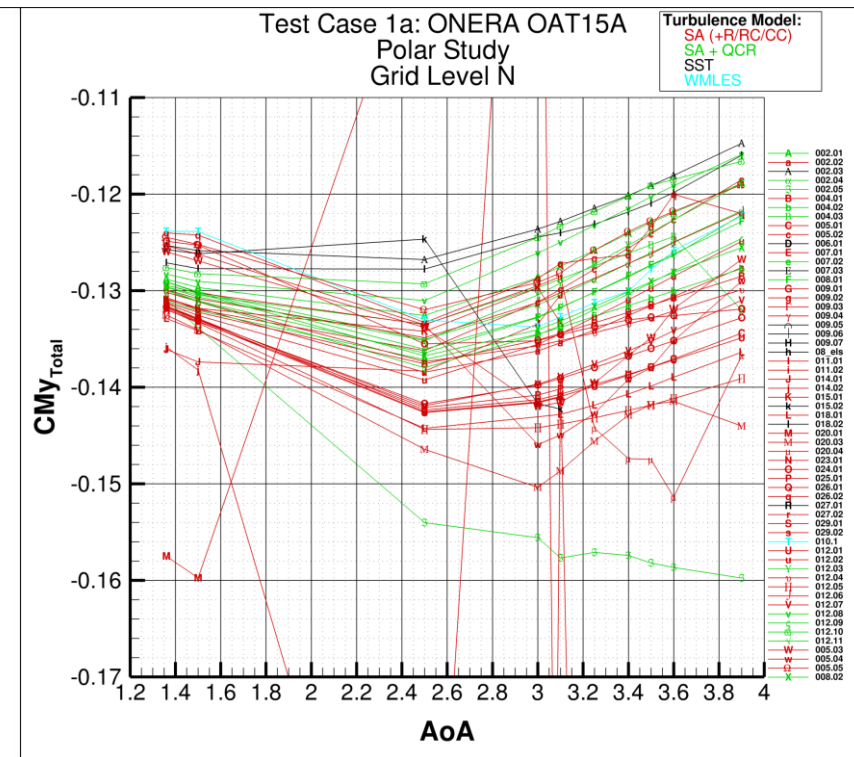
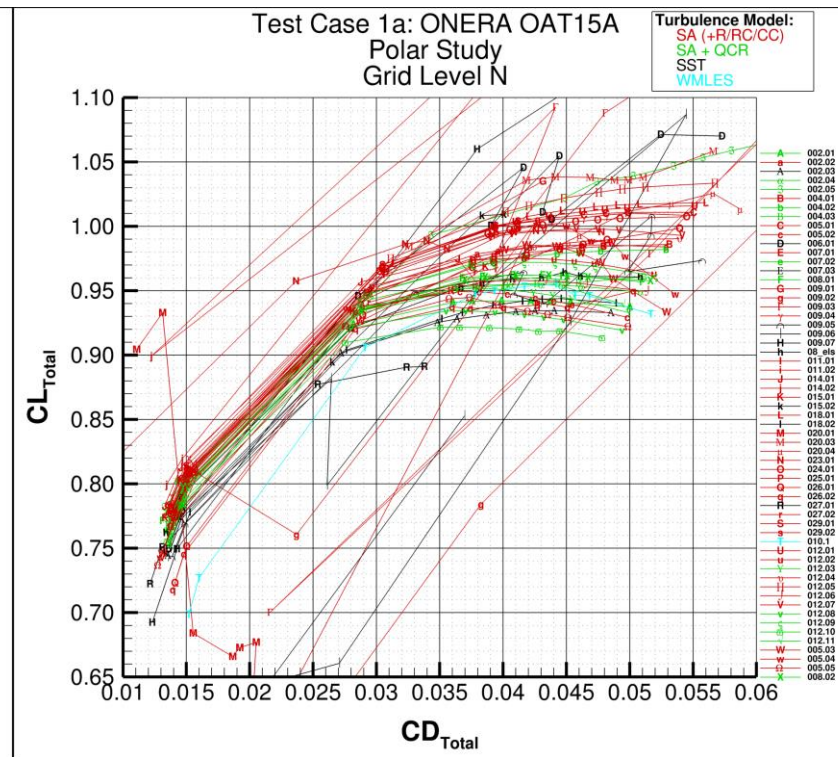
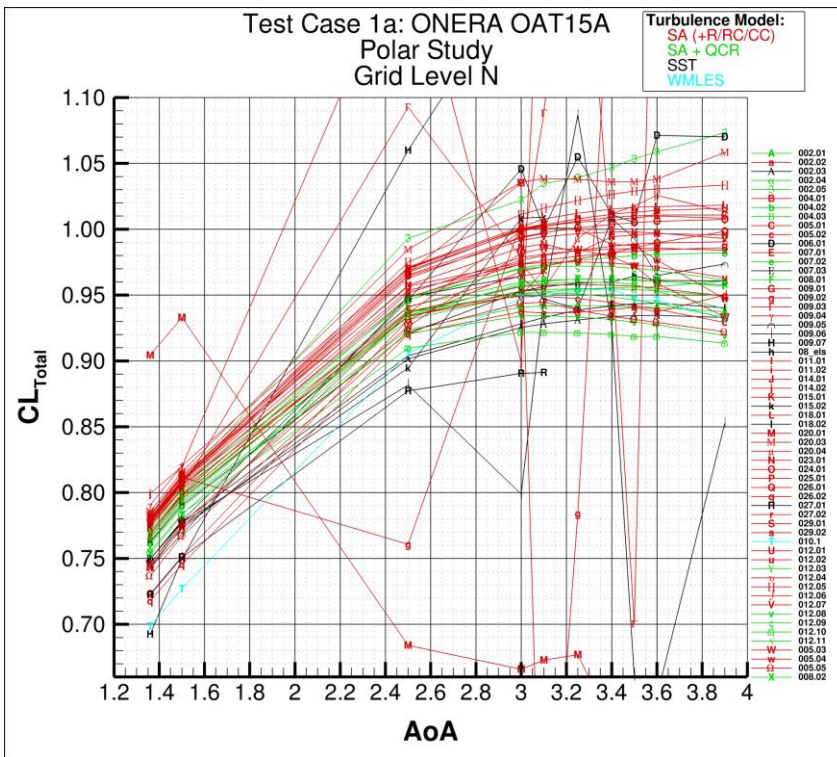
- Lift, Drag, Pitching Moment Polars
  - Finest Submitted Grid Level



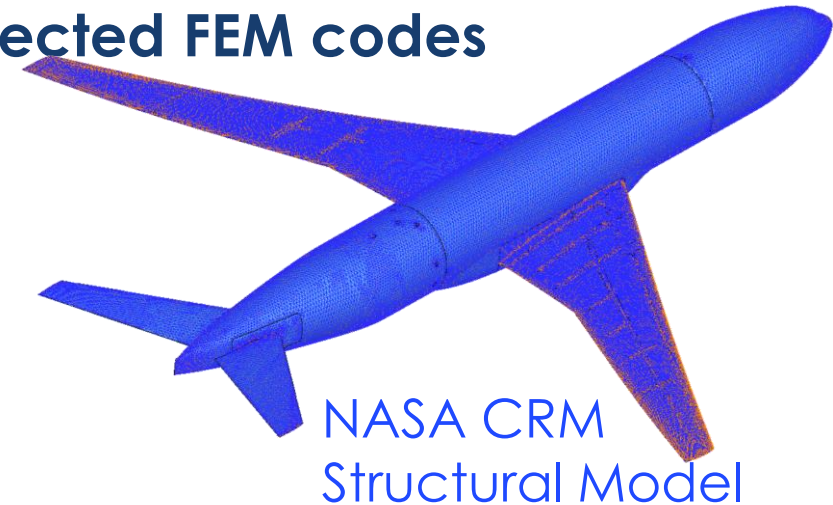


# Test Case 1a: Results

- Lift, Drag, Pitching Moment Polars
  - Finest Submitted Grid Level



- **Validation of Structural Model for NASA CRM**
  - Tap Test planned for comparison to normal mode solutions of FEM models
  - Static Loads Tests will be conducted to compare deflection measurements (and maybe twist) to Linear Static FEM solutions
- **Users are encouraged to employ best practices for selected FEM codes**
- **Settings**
  - Linear Eigenvalue Analysis (e.g. NASTRAN<sup>®</sup> SOL103)
- **Conditions**
  - Rigid suspension at sting
- **Grid**
  - MSC NASTRAN<sup>®</sup> solid 4-node tetrahedral finite-element structural model
  - Model consists of  $6.8 \cdot 10^6$  elements,  $4.1 \cdot 10^6$  degrees-of-freedom
  - Supplied by NASA Langley's Configuration Aerodynamics Branch
  - Wind tunnel sting will be added as beam model



# Test Case 2a: Wing/Body Deformation

- **CFD/FEM start from unloaded (wind-off) geometry/grid**
- **CRM Wing/Body**
  - Reynolds numbers: 5M (LoQ) [Available: 5M(LoQ),20M(LoQ),20M(HiQ),30M(HiQ)]
  - Mach Number: 0.85 [Available: 0.70, 0.85, 0.87]
  - Angle of Attack: 3.00 deg [Available: -3.0 – 12.0 deg]
- **Committee-supplied**
  - NASA CRM geometry in jig/unloaded condition
    - Trip location, if tested (optional to use)
  - MSC NASTRAN<sup>®</sup> finite-element model of the NASA CRM
  - Grid Family (L1:Tiny/L2:Coarse/L3:Medium/L4:Fine/L5:eXtra-fine/L6:Ultra-fine)
- **Comparison metrics**
  - Forces / Moments
  - Sectional Twist / Deformation
  - Sectional  $C_p$  distribution

# Test Case 2b: Wing/Body Deformation (polar)

- **CFD/FEM start from unloaded (wind-off) geometry/grid**
- **CRM Wing/Body**
  - Available Reynolds numbers: 5M (LoQ), 20M (LoQ), 20M (HiQ), 30M (HiQ)
  - Range of Mach numbers: 0.70, 0.85, 0.87 ( $M_{\text{cruise}} = 0.85$ )
  - Range of Angles of attack: -3.0 – 12.0 deg ( $AOA_{\text{cruise}} \sim 2.75\text{-}3.00$  deg)
- **Committee-supplied**
  - NASA CRM geometry in jig/unloaded condition
    - Trip location, if tested (optional to use)
  - MSC NASTRAN<sup>®</sup> finite-element model of the NASA CRM
  - Grid Family (L1:Tiny/L2:Coarse/L3:Medium/L4:Fine/L5:eXtra-fine/L6:Ultra-fine)
- **Comparison metrics**
  - Forces / Moments
  - Sectional Twist / Deformation
  - Sectional  $C_p$  distribution

# Test Case 3: Wing/Body/Nacelle/Pylon

- **CFD/FEM start from unloaded (wind-off) geometry/grid**
- **CRM Wing/Body/Nacelle /Pylon**
  - Available Reynolds numbers: 5M (LoQ)
  - Range of Mach numbers: 0.70, 0.85, 0.87 ( $M_{\text{cruise}} = 0.85$ )
  - Range of Angles of attack: -3.0 – 12.0 deg ( $AOA_{\text{cruise}} \sim 2.75\text{-}3.00$  deg)
- **Committee-supplied**
  - NASA CRM geometry in jig/unloaded condition
    - Trip location, if tested (optional to use)
  - MSC NASTRAN<sup>®</sup> finite-element model of the NASA CRM
  - Grid Family (L1:**T**iny/L2:**C**oarse/L3:**M**edium/L4:**F**ine/L5:**eX**tra-fine/L6:**U**ltra-fine)
- **Comparison metrics**
  - Forces / Moments
  - Sectional Twist / Deformation
  - Sectional  $C_p$  distribution



- **What level of accuracy can transonic wing deformations be calculated?**
- **What is the uncertainty in configuration force/moments due to aeroelastic deformation uncertainty?**
- **What are the most efficient/accurate methods for coupling the aero/structural computations?**
  - What are the computational time/accuracy savings between using a full fidelity vs reduced beam structural model?
  - Do modal solutions compare well to direct fluid-structure mapping solutions?
  - Does a full vs symmetry plane solution result in different solutions?
- **What accuracy is lost by using a “lower fidelity” aerodynamic?**

# Nominal Schedule

- **June, 2024**
  - First Working Group Meeting ✓
  - ONERA OAT15A geometry release ✓
- **July, 2024**
  - ONERA OAT15A grids released ✓
  - AVIATION in-person meeting ✓
- **November, 2024**
  - All workshop virtual meeting (11/8) ✓
- **January, 2025**
  - SciTech Forum: Mini Workshop 1 ✓
  - CRM Grids Available
- **March, 2025**
  - FEM Validation Data released
- **July, 2025**
  - AVIATION in-person meeting
  - (Special Session: ONERA OAT15a?)
- **Summer/Fall, 2025 (?)**
  - Mini Workshop 2
- **January, 2026**
  - SciTech in-person meeting
- **February, 2026**
  - Delivery of final data set (perhaps alternate submissions prior to this date)
- **June, 2026**
  - Workshop in San Diego, CA

# Working Group Meeting Cadence

- **Currently set up for 10:00 Eastern time on third Friday of each month**
  - A suitable meeting time is very difficult for global participants
  - Recurring meeting invite sent
  
- **Next meeting: Friday, February 21<sup>st</sup>**
  - Please contact [ben.j.rider2@boeing.com](mailto:ben.j.rider2@boeing.com) if you are interested to present grids or solutions

